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# Size- and speed-dependent mechanical behavior in living mammalian cytoplasm

Jiliang Hu<sup>a,b</sup>, Somaye Jafari<sup>c</sup>, Yulong Han<sup>a</sup>, Alan J. Grodzinsky<sup>a,d</sup>, Shengqiang Cai<sup>c,1</sup>, and Ming Guo<sup>a,1</sup>

<sup>a</sup>Department of Mechanical Engineering, Massachusetts Institute of Technology, Cambridge, MA 02139; <sup>b</sup>Department of Engineering Mechanics, Tsinghua University, Beijing 100084, People's Republic of China; <sup>c</sup>Department of Mechanical and Aerospace Engineering, University of California, San Diego, La Jolla, CA 92093; and <sup>d</sup>Department of Biological Engineering, Massachusetts Institute of Technology, Cambridge, MA 02139

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Active transport in the cytoplasm plays critical roles in living cell physiology. However, the mechanical resistance that intracellular compartments experience, which is governed by the cytoplasmic material property, remains elusive, especially its dependence on size and speed. Here we use optical tweezers to drag a bead in the cytoplasm and directly probe the mechanical resistance with varying size  $a$  and speed  $V$ . We introduce a method, combining the direct measurement and a simple scaling analysis, to reveal different origins of the size- and speed-dependent resistance in living mammalian cytoplasm. We show that the cytoplasm exhibits size-independent viscoelasticity as long as the effective strain rate  $V/a$  is maintained in a relatively low range ( $0.1 \text{ s}^{-1} < V/a < 2 \text{ s}^{-1}$ ) and exhibits size-dependent poroelasticity at a high effective strain rate regime ( $5 \text{ s}^{-1} < V/a < 80 \text{ s}^{-1}$ ). Moreover, the cytoplasmic modulus is found to be positively correlated with only  $V/a$  in the viscoelastic regime but also increases with the bead size at a constant  $V/a$  in the poroelastic regime. Based on our measurements, we obtain a full-scale state diagram of the living mammalian cytoplasm, which shows that the cytoplasm changes from a viscous fluid to an elastic solid, as well as from compressible material to incompressible material, with increases in the values of two dimensionless parameters, respectively. This state diagram is useful to understand the underlying mechanical nature of the cytoplasm in a variety of cellular processes over a broad range of speed and size scales.

cell mechanics | poroelasticity | viscoelasticity | cytoplasmic state diagram

The cytoplasm of living mammalian cells is a crowded, yet dynamic, environment (1). There are continuous intracellular movements that are vital for cell physiology, such as transport of vesicles and other organelles. While biological motors and other enzymatic processes provide key driving forces for these activities, the mechanical properties of the cytoplasm are crucial for determining the mechanical resistance that cellular compartments experience. Indeed, both the active driving force and appropriate mechanical environment are critical for shaping the living cellular machinery. However, while the force that molecular motors generate both individually and collectively has been extensively studied (2, 3), the mechanical properties of the cytoplasmic environment remain elusive. In addition, the impact of object size and velocity on the mechanical resistance that active forces need to overcome to enable transport remains unclear. Such characterization is essential for understanding the physical environment and numerous key dynamic processes inside living cells.

The cytoplasm is composed of cytoskeletal networks and many proteins, as well as organelles and vesicles. Materials with such complex microstructure are expected to display time-dependent or frequency-dependent properties (4). Indeed, it has been revealed by many experimental approaches that the mechanical properties of living cells exhibit clear frequency dependency (5, 6); the cell response follows a power-law rheology behavior within a broad frequency range (3, 7, 8). A common view is that cells are viscoelastic materials (9–13), and the observed mechanical properties depend on the timescale over which the deformation occurs during the measurement. One important feature of a viscoelastic material

is that its mechanical property does not depend on any length scales of the observation (14). Interestingly, it has recently been demonstrated that living cells may also behave like a poroelastic gel at short timescales (15–17); the stress relaxation of cells can be entirely determined by migration of cytosol through cytoskeletal networks. In the framework of poroelasticity, the measured mechanical property strongly depends on the size of the probe, as it takes a longer time for cytosol to move over a longer distance, therefore the stress relaxes slower. The size-dependent poroelastic behavior is in direct contrast to viscoelasticity whose relaxation is a material property and is independent of probe size, set by the time-dependent response of the materials' macromolecular and supramolecular constituents. More importantly, most of previous attempts to study cell mechanics probe cells from the exterior, such as by using atomic force microscopy or an optical stretcher, and thus the measurement depends more on the stiff actin-rich cell cortex rather than on the much softer cytoplasm (13, 15, 18). Therefore, it remains unclear if viscoelasticity or poroelasticity better describes the rate-dependent resistance of the cytoplasm of living mammalian cells, or if both are required.

In this paper, we use optical tweezers to drag a plastic bead in the cytoplasm of a living mammalian cell and directly measure the force (denoted by  $F$ ) and displacement (denoted by  $x$ ) relationship, which reflects the mechanical behavior of the cytoplasm. Considering both viscoelasticity and poroelasticity, we identify two independent dimensional parameters in the experiments:  $V/a$  and  $Va$ , where  $V$  and  $a$  represent the speed and diameter of the probe bead, respectively. Using these two control parameters, and through a combination of experimental measurement and scaling analysis, we

## Significance

Although the driving force generated by motor proteins to deliver intracellular cargos is widely studied, the mechanical nature of cytoplasm, which is also important for intracellular processes by providing mechanical resistance, remains unclear. We use optical tweezers to directly characterize the resistance to transport in living mammalian cytoplasm. Using scaling analysis, we successfully distinguish between the underlying mechanisms governing the resistance to mechanical deformation, that is, among viscosity, viscoelasticity, poroelasticity, or pure elasticity, depending on the speed and size of the probe. Moreover, a cytoplasmic state diagram is obtained to illustrate different mechanical behaviors as a function of two dimensionless parameters; with this, the underlying mechanics of various cellular processes over a broad range of speed and size scales is revealed.

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<sup>1</sup>To whom correspondence may be addressed. Email: s3cai@ucsd.edu or guom@mit.edu.

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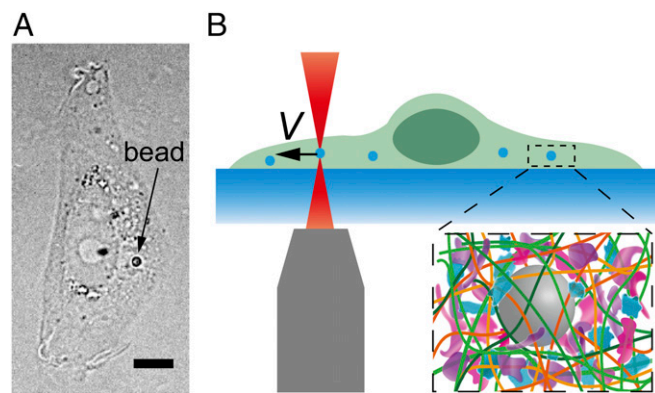
reveal different origins of cytoplasmic resistance, ranging from viscous, viscoelastic, and poroelastic to pure elastic. Finally, we classify different cytoplasmic mechanical behaviors in an overall state diagram, which illustrates different origins of mechanical resistance of a variety of physiological processes in cells with different characteristic size and speed.

## Results and Discussion

To investigate the mechanical resistance that intracellular objects experience within a living mammalian cytoplasm we deliver micrometer-sized polystyrene beads into living normal rat kidney epithelial cells (NRK) through endocytosis (Fig. 1*A*). These beads, with sizes ranging from 0.5  $\mu\text{m}$  to 1.5  $\mu\text{m}$ , distribute randomly inside the cell and are much larger than the typical cytoskeletal mesh size [ $\sim 50$  nm (19)]; these beads can thereby probe the cytoplasm modeled as a continuous medium. We then use optical tweezers to trap and pull a bead unidirectionally with a constant speed toward the cell boundary, as illustrated in Fig. 1*B* and Movie S1. To avoid any interactions with the mechanically distinct cell cortex and nucleus we only use beads that are positioned greater than 1.5  $\mu\text{m}$  away from the cell boundary, and away from both the thin lamellar region and the nucleus. The beads are pulled unidirectionally at a constant speed; thus, the intracellular resistance force on the bead in the direction of motion equals the measured pulling force. A force-vs.-displacement curve of the cytoplasm is then obtained (Fig. S1*A*). To compare measurements of different bead sizes we normalize the force as  $F/S$  and the displacement as  $x/a$ , where  $S$  is the cross-sectional area and  $a$  is the diameter of the bead, and thus obtain a normalized force-displacement curve.

To understand the mechanical resistance in the cytoplasm we assume that the resistance force experienced by the bead is mainly due to the restoring force from the deformed cytoskeleton and the inhomogeneously distributed pore pressure in the cytoplasm. Deformation of the cytoskeleton structure itself is typically viscoelastic, which can result from cytoskeletal structure rearrangement and bond fracture of proteins (20). The kinetics of viscoelasticity can be characterized by intrinsic relaxation timescales or time spectra (21, 22) that are independent of loading conditions, such as bead diameter and speed. The local deformation of the cytoplasm also results in an inhomogeneous distribution of pore pressure in the porous structure formed by the cytoskeleton due to poroelasticity (15, 23). To reach a rehomogenization of pore pressure distribution, the intracellular fluid flows over characteristic distances related to bead size, with characteristic poroelastic relaxation time  $a^2/D$ ;  $D$  is the effective poroelastic diffusivity of the cytosol and scales as  $D \sim E\kappa$  (23), where  $E$  is the equilibrium elastic modulus of the cytoplasm and  $\kappa$  is the permeability defined as the flux of cytosol through cytoskeletal network under unit pressure gradient. We thus take both viscoelasticity and poroelasticity into consideration when analyzing the mechanical resistance of the cytoplasm. Both viscoelastic relaxation times and effective poroelastic diffusivity are considered as constants for NRK cells in the following discussion.

In our experiments there is only one timescale associated with the loading condition, which is  $a/V$ . Based on simple scaling analysis, the relationship between the resistant force and bead displacement,  $F = f(E, \tau_i, D, \nu, a, x, V)$ , can be transformed to a dimensionless form,  $F/ES = f(x/a, Va/D, V\tau_i/a, \nu)$ , where  $S$  is the cross-sectional area of the bead,  $\nu$  is the equilibrium Poisson's ratio of the cytoplasm, and  $\tau_i$  represents a series of characteristic viscoelastic timescales. For a certain cell type,  $E$ ,  $D$ ,  $\tau_i$ , and  $\nu$  are constants. Here,  $V\tau_i/a$  ( $i = 1, 2, 3, \dots$ ) are dimensionless parameters denoting the ratio of the characteristic viscoelastic timescales to the experimental timescale, which is known as the Deborah number (24).  $Va/D$  is the ratio of the characteristic poroelastic timescale to the experimental timescale. As discussed above, when the observed rate-dependent mechanical behavior is only due to viscoelasticity, and a constant  $V/a$  is maintained, the measured relations between  $F/S$  and  $x/a$  should collapse to one curve; when the observed rate-dependent



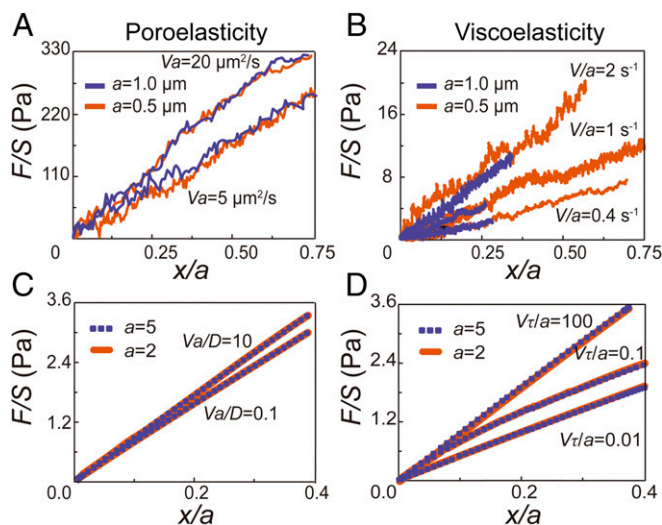
**Fig. 1.** Experimental setup measuring the mechanical resistance in living mammalian cytoplasm. (A) Bright-field image of an NRK cell with a 1- $\mu\text{m}$ -diameter particle inside. (Scale bar, 5  $\mu\text{m}$ .) (B) Schematic showing the experimental setup. A probe bead is dragged at a constant speed toward the cell boundary to obtain a force-displacement curve. (Inset) The crowded environment around the bead in cells.

behavior is only due to poroelasticity, and a constant  $Va$  is maintained, the measured relations should collapse to one curve.

To validate the ability of our experimental approach to distinguish between viscoelastic and poroelastic behaviors we perform unidirectional particle stretching within classical poroelastic and viscoelastic materials having known material properties. To test poroelastic behavior, we use polyacrylamide (PA) (3% acrylamide and 0.05% bis-acrylamide cross-linker), a hydrogel having covalently cross-linked networks demonstrated to have linear elastic behavior over a broad range of frequencies (25). However, when the gel is subjected to a high-enough strain rate deformation, fluid flow within the gel network affects material resistance to the applied deformation, and the rate dependence is well captured by linear poroelasticity theory (26). We premix beads of two different sizes (0.5- $\mu\text{m}$  and 1- $\mu\text{m}$  diameter) and perform unidirectional pulling at relatively high speeds (5, 10, 20, and 40  $\mu\text{m/s}$ ). We find that the measured normalized force-displacement curves are close to each other when  $Va$  is a constant (Fig. 2*A*). Moreover, higher values of  $Va$  yield larger stresses at the same strain, consistent with the behavior of poroelastic materials. In addition, according to the analytical solution of the inclusion problem of a spherical rigid inclusion within an elastic medium (27), the Young's modulus of the medium  $E$  can be obtained as  $E = [(5 - 6\nu)(1 + \nu)/24(1 - \nu)]E_A$ , where  $\nu$  is the Poisson's ratio and  $E_A$  is the apparent modulus measured as the average slope of the normalized force-displacement curve from 0 to 10% normalized displacement. Using a Poisson's ratio of 0.457 (28), the calculated elastic modulus of our PA gel is  $\sim 80$  Pa (Fig. 2*A*), in agreement with our bulk rheology measurements on the same gel (Fig. S2).

To test if stress strain curves with the same  $V/a$  collapse in the viscoelastic regime we use ionic cross-linked alginate gel, made of 5 mg/mL alginate solution cross-linked with 3 mM calcium sulfate. The viscoelastic behavior of alginate gel has been well characterized in a broad frequency range corresponding to low-enough strain rates (29). In this case, beads are pulled at a range of relatively low speeds (0.4, 0.8, 1, 2, and 4  $\mu\text{m/s}$ ) for which viscoelasticity dominates stress-strain behavior. Indeed, we find that at constant  $V/a$  the measured normalized force-displacement curves are close to each other (Fig. 2*B*). For the same bead size, higher pulling speed results in a greater resistant force, also consistent with the response of most viscoelastic materials. When the strain rate is high, stresses in the material do not have time to relax. These results demonstrate that our method can indeed distinguish poroelasticity and viscoelasticity in a material.





**Fig. 2.** Validation of the scaling argument through experiments in classical materials and with finite element simulation. (A) Normalized force-displacement curves obtained in a classical poroelastic material, PA gel, by dragging beads with 1  $\mu\text{m}$  (blue lines) and 0.5  $\mu\text{m}$  (orange lines) in diameter at different speeds. Curves with the same  $Va$  (20  $\mu\text{m}^2/\text{s}$  and 5  $\mu\text{m}^2/\text{s}$ , respectively) are close to each other. (B) Normalized force-displacement curves obtained in a classical viscoelastic material, alginate gel (5 mg/mL alginate cross-linked with 3 mM calcium sulfate), by dragging beads with 1  $\mu\text{m}$  (blue lines) and 0.5  $\mu\text{m}$  (orange lines) in diameter at different speeds. Curves with the same  $V/a$  (2, 1, and 0.4  $\text{s}^{-1}$ , respectively) are close to each other. Each force displacement curve shown in A and B is averaged over at least 20 individual experiments. (C and D) Finite element simulation of dragging a bead in a large cubic poroelastic material (C) and viscoelastic material (D). Two dimensionless bead sizes are used, 5/5,000 of the overall sample length (orange lines), and 2/5,000 of the sample length (purple dashed lines). (C) If the material is defined as poroelastic, curves with the same  $Va/D$  (10 and 0.1, respectively) collapse. (D) If the material is defined as viscoelastic, curves with the same  $Vt/a$  (100, 0.1, and 0.01, respectively) collapse.

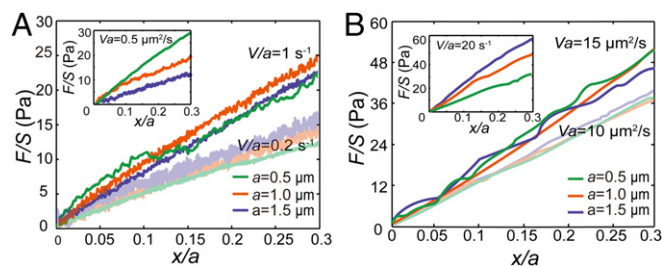
In addition, we have also performed finite element simulations using ABAQUS ([www.3ds.com](http://www.3ds.com)) to verify our scaling analysis. In the simulation, a rigid bead is embedded within an elastic solid, which is much larger than the bead. A constant velocity is applied to the bead. The resistant force exerted on the bead is then computed. In the simulation, the elastic solid is defined as either a viscoelastic material [using a Prony series (30)] or a linear poroelastic material. As expected, our numerical simulations again confirm the scaling analysis (Fig. 2 C and D).

We next apply this method in the cytoplasm of living NRK cells. We measure the normalized force-displacement curves at different loading speeds and with three different bead sizes (0.5, 1, and 1.5  $\mu\text{m}$ ). We find that the cytoplasm's mechanical behavior strongly depends on the two dimensional numbers,  $V/a$  and  $Va$ , in two ranges of effective strain rate. The cytoplasm is viscoelastic at low effective strain rates ( $0.1 \text{ s}^{-1} < V/a < 2 \text{ s}^{-1}$ ), as the normalized force-displacement curves are close to each other for measurements with the same  $V/a$  (e.g., 1, 0.5, and 0.2  $\text{s}^{-1}$ , Fig. 3A and Fig. S3A). Within this regime, when we compare measurements with the same  $Va$  instead (e.g., 0.5  $\mu\text{m}^2/\text{s}$ ) they clearly separate from each other (Fig. 3A, Inset). Through similar analysis, we find that the cytoplasm appears poroelastic under high effective strain rate ( $5 \text{ s}^{-1} < V/a < 80 \text{ s}^{-1}$ ), as the normalized force-displacement curves are close to each other for measurements with the same  $Va$  (e.g., 20, 15, and 10  $\mu\text{m}^2/\text{s}$ , Fig. 3B and Fig. S3B). Again, within this regime, when we compare measurements with the same  $V/a$  (e.g., 20  $\text{s}^{-1}$ ) they are distinguished from each other (Fig. 3B, Inset). Moreover, when the effective strain rate is reduced further ( $V/a < 0.1 \text{ s}^{-1}$ ) the resistance force remains roughly a constant with increasing displacement (Fig. S4). This is a typical feature of a

viscous fluid with an effective viscosity, estimated here to be  $12.1 \pm 6.3 \text{ Pa}\cdot\text{s}$  ( $n = 15$ , mean  $\pm$  SD), consistent with previous measurements (10, 31). Similar results are observed using HeLa cells (Fig. S5).

We also note that when the probe size becomes comparable to or even smaller than the mesh size of the cytoskeletal network it is not valid anymore to view the cytoplasm as a continuum and use the above scaling analysis to study the mechanical interaction between the bead and the cytoplasm. However, most common cytoplasmic organelles, such as vesicles and mitochondria, are much larger than typical cytoplasmic mesh size and are in fact comparable in size to the beads we use here. Therefore, our measurements here provide direct insights into understanding the mechanical resistance that common organelles experience in living cells.

The cytoplasm of mammalian cells is a porous structure formed by cytoskeletal networks and other proteins, filled with cytosol (15). Our results demonstrate that living mammalian cytoplasm exhibits viscous fluid behavior, viscoelasticity and poroelasticity, respectively, with different combinations of bead size and speed. Under high-enough effective strain rates the characteristic time for moving over one bead diameter is comparable to the time needed for cytosol to migrate around the bead; this leads to the observed rate dependence induced by poroelasticity. However, at low-enough effective strain rates, the resulting slow cytosol motion is accompanied by essentially instantaneous rehomogenization of pore pressure; thus, any residual rate-dependent resistance to bead motion is due to viscoelastic behavior of the cytoskeletal network. Furthermore, when the bead speed is extremely low the cytoplasm behaves as a viscous fluid, since at such very long timescales the cytoskeleton has enough time to depolymerize and reform, and the fully relaxed cytoplasm can thereby undergo viscous flow upon loading. In our experiments, the poroelastic relaxation time of the cytoplasm is about 0.02–0.1 s, estimated from the range of effective strain rates at which poroelasticity is observed (Fig. 3B); this is much shorter than the apparent viscoelastic relaxation time,  $\tau = 0.79 \pm 0.13 \text{ s}$ , measured in the cytoplasm of NRK cells (Fig. S1B).  $\tau$  is obtained through single-term exponential fitting of the relaxation curve measured in the cytoplasm. Although the cytoplasm may have a spectrum of relaxation times (21), our exponential fitting with a single characteristic time agrees reasonably well with the experimental data (Fig. S1B); this indicates that even though there is a spectrum of relaxation times it does have a dominating range in



**Fig. 3.** Normalized force-displacement curves measured in the cytoplasm of NRK cells show that the cytoplasm exhibits viscoelasticity under small effective strain rate and exhibits poroelasticity under large effective strain rate. Each curve shown here is averaged over at least 20 individual experiments. (A) Under low effective strain rate, the normalized force-displacement curves obtained with different bead sizes (0.5, 1, and 1.5  $\mu\text{m}$ ) are close to each other when the same  $V/a$  is maintained (e.g., 1  $\text{s}^{-1}$  and 0.2  $\text{s}^{-1}$ ). (Inset) Normalized force-displacement curves with different bead sizes are clearly separated when we compare experiments with the same  $Va$  in the low-speed regime. (B) Under high effective strain rate, the normalized force-displacement curves with different bead sizes (0.5, 1, and 1.5  $\mu\text{m}$ ) are close to each other when the same  $Va$  is maintained (e.g., 15  $\mu\text{m}^2/\text{s}$  and 10  $\mu\text{m}^2/\text{s}$ ). (Inset) Normalized force-displacement curves with different bead sizes are clearly separated when we compare experiments with the same  $V/a$  in the high-speed regime.

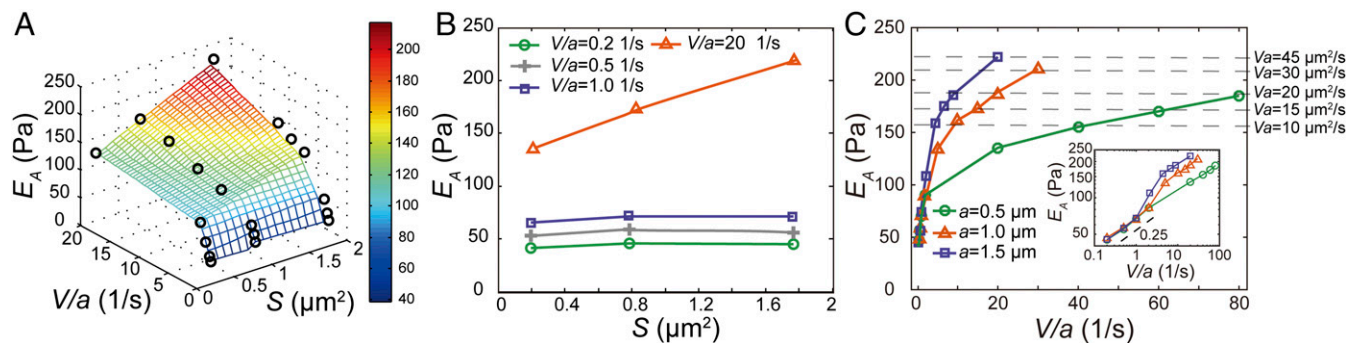
timescale which shares the same order of magnitude with the fitted apparent relaxation time  $\tau$ . During this apparent relaxation time, viscoelastic resistance in the cytoplasm relaxes markedly. For the convenience of discussion but without losing generality we use the apparent relaxation time  $\tau$ , instead of the time spectrum  $\tau_i$  ( $i = 1, 2, 3, \dots$ ) in the following discussion on cytoplasmic viscoelasticity. The poroelastic diffusion coefficient of the cytosol, estimated from the experimental timescale,  $T (= a/V)$ , at which we observe the poroelastic regime, is  $D = a^2/T \approx 50 \mu\text{m}^2/\text{s}$ ; this is consistent with previous measurements in mammalian cells (15). Our measurements demonstrate that cytoplasmic mechanical properties have different origins at different timescales: viscoelastic and viscous behavior due to relaxation and reorganization of the cytoplasmic structure dominate cytoplasmic mechanics at long timescales, while poroelasticity due to fluid–solid (cytosol–cytoskeleton) frictional interactions and energy dissipation dominate at short timescales.

To investigate the contribution of the cytoskeletal network to the mechanical nature of the cytoplasm we use  $5 \mu\text{g/mL}$  cytochalasin D to depolymerize F-actin structures, a major part of the cytoskeleton, then apply unidirectional stretching. We observe a clear decrease in the characteristic viscoelastic timescale  $\tau$  and a marked increase of the effective poroelastic diffusivity  $D$  in the cytoplasm (Fig. S6), thereby decreasing the poroelastic relaxation time. We note that the poroelastic diffusion coefficient, which describes the effective diffusion of the fluid within a porous medium caused by internal pressure gradients, is different from the usual solute diffusion coefficient which accounts for the collective motion of solutes in response to concentration gradients in the solvent medium. Depolymerizing F-actin causes an increase of the cytoskeletal mesh size and porosity in the cytoplasm, and hence increases the poroelastic diffusivity. The decrease in the viscoelastic timescale is likely to be due to the loss of the friction among F-actin structures and other cytoplasmic components (32), or other actin-associated activities. Thus, disrupting the F-actin network expedites both the cytoplasmic viscoelastic relaxation and the diffusion of cytosol when the cell is deformed. As a result, the critical effective strain rate,  $V/a$ , that initiates poroelastic behavior increases. Moreover, the transition effective strain rate from a seemingly viscous fluid behavior to a viscoelastic material also increases.

It has also been shown that the biological activity of molecular motors largely affects the mechanical properties of reconstituted cytoskeletal networks (33, 34) and increases cytoplasmic fluidity in bacteria (35). To investigate how such biological activity influences

the mechanical behavior of the cytoplasm of mammalian cells we perform force-relaxation tests in HeLa cells with myosin II motors inhibited by blebbistatin treatment or with depletion of ATP. We find that the characteristic relaxation time in the cytoplasm significantly increases from  $0.31 \pm 0.08 \text{ s}$  in normal HeLa cells to  $0.50 \pm 0.20 \text{ s}$  in blebbistatin-treated cells and further increases to  $0.73 \pm 0.30 \text{ s}$  in ATP-depleted cells (Table S1). Both blebbistatin treatment and ATP depletion slow down cytoplasmic reorganization, thus increasing the characteristic viscoelastic relaxation time  $\tau$ . This observation is consistent with previous results with reconstituted cytoskeletal networks and in bacteria cytoplasm (33, 35). This increase in  $\tau$  causes a decrease in the transition effective strain rate  $V/a$  from a viscous fluid to a viscoelastic gel. These results indicate that both the cytoskeleton and other active cellular components affect the mechanical response of the cytoplasm by influencing cytoplasmic mechanical parameters such as viscoelastic relaxation time and poroelastic diffusivity.

To quantitatively characterize the mechanical resistance that an object experiences when moving in the cytoplasm we calculate the rate-dependent apparent modulus of the cytoplasm from the slope of the stress-vs.-strain curve. This rate-dependent modulus can be converted to the storage and loss moduli based on certain rheological models and the Boltzmann superposition principle (32). Although the storage and loss moduli are more often adopted to describe soft materials and complex fluids (3, 36), we adopt this apparent modulus to characterize the mechanical property of the cytoplasm, since it is most relevant to the rate- and size-dependent resistance force that a particle may experience in the cytoplasm. Interestingly, we find that all of the normalized force-displacement curves measured in the cytoplasm are rather linear when the normalized displacement remains relatively small, (i.e., smaller than the radius of the bead). Thus, an apparent elastic modulus,  $E_A$ , is calculated as the average slope from 0 to 10% strain. Interestingly, we find that the apparent elastic modulus depends on both probe size and loading speed, as shown in Fig. 4A. To reveal the dependency of  $E_A$  on the probe size we project this 3D plot onto 2D axes,  $E_A$  vs.  $S$ . For a small effective strain rate ( $0.1 \text{ s}^{-1} < V/a < 2 \text{ s}^{-1}$ ),  $E_A$  remains constant for varying probe size because viscoelasticity dominates this regime (Fig. 4B). However, for a large effective strain rate ( $V/a > 5 \text{ s}^{-1}$ ),  $E_A$  increases with probe size (Fig. 4B); this is indeed because poroelasticity starts to contribute to the measurement of the apparent modulus, and it becomes increasingly difficult for the differential pore pressure to be relaxed as the probe size increases.



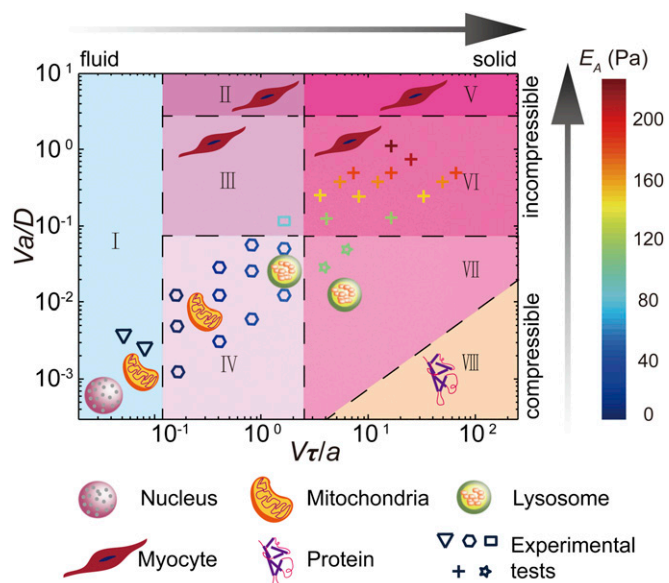
**Fig. 4.** Cytoplasmic modulus under different effective strain rates and probe sizes. (A) Dependence of the apparent cytoplasmic modulus on normalized loading speed and probe size. Each modulus value (black circles) is averaged over at least 20 experiments; the SE bar has a length smaller than the size of the symbols in the plot. The 3D surface is obtained by piecewise linear interpolation of the measured apparent cytoplasmic modulus ( $E_A$ ). The color of the surface represents the value of  $E_A$ . (B)  $E_A$  at different loading conditions does not change with the area of the probe bead at low effective strain rate regime, since viscoelasticity is dominating in this regime. However,  $E_A$  increases with the area of the bead at the high effective strain rate regime, since poroelasticity is dominating in this regime. (C)  $E_A$  is solely determined by  $V/a$  at low effective strain rate regime ( $0.1 \text{ s}^{-1} < V/a < 2 \text{ s}^{-1}$ ); this reinforces that  $V/a$  is the control parameter of the mechanical resistance at the low effective strain rate regime where viscoelasticity dominates. At the high effective strain rate regime ( $V/a > 5 \text{ s}^{-1}$ ),  $E_A$  obtained with different probe size starts to deviate even at the same  $V/a$ . Instead,  $E_A$  has the same value when the same  $V/a$  is maintained (indicated by the horizontal dashed lines); this reinforces that  $V/a$  is the control parameter of the resistance at the high effective strain rate regime where poroelasticity dominates. (Inset) The logarithmic plot of the dependence of  $E_A$  on  $V/a$ , which exhibits a seeming power-law behavior with a power of  $\sim 0.25$  at the low-speed regime.



Different origins of cytoplasmic elasticity can be further revealed when we plot the apparent cytoplasmic modulus as a function of  $V/a$  (Fig. 4C). The apparent modulus from all measurements follows exactly the same trend at low effective strain rate regardless of bead size;  $E_A$  is solely determined by  $V/a$  at this regime, confirming that the resistant force is mainly due to viscoelasticity. Interestingly, in this regime the measured dependence of  $E_A$  on effective strain rate is also consistent with previously observed power-law rheology with a power around 0.2 (3, 7). However, when effective strain rate becomes large, no obvious correlation between the apparent modulus and the number  $V/a$  can be seen. Instead, when  $V/a$  is a constant, we obtain the same modulus, as indicated by the dashed lines in Fig. 4C;  $E_A$  remains the same even if the value of  $V/a$  changes by orders of magnitude. In this regime, the rate dependence of the resistant force is mainly contributed by the poroelasticity of the cytoplasm. The transition between these two regimes is around  $V/a = 3 \text{ s}^{-1}$ ; both viscoelasticity and poroelasticity contribute at this transition region (Fig. S7). The different dependency of the apparent modulus on  $V/a$  and  $Va$  in different regimes reinforces the conclusion that viscoelasticity dominates the size-independent (for a fixed effective strain rate,  $V/a$ ) mechanical behavior under low effective strain rate when the experimental timescale  $a/V$  is comparable to the viscoelastic timescale  $\tau$ , namely  $V\tau/a \sim 1$ , while poroelasticity dominates the size-dependent (for a fixed effective strain rate,  $V/a$ ) mechanical behavior under high effective strain rate when the experimental timescale is comparable to the poroelastic timescale  $a^2/D$ , namely  $Va/D \sim 1$ .

Finally, we summarize different cytoplasmic mechanical behaviors in a state diagram as a function of two dimensionless parameters,  $V\tau/a$  and  $Va/D$  (Fig. 5). Under different loading conditions, the mechanical response of the cytoplasm can be divided into eight types, corresponding to eight sections on the state diagram. When  $V\tau/a \ll 1$  (section I), the cytoplasm behaves as a viscous fluid. As  $V\tau/a \sim 1$  (sections II–IV), viscoelasticity contributes to the rate-dependent mechanical properties of cells. When  $V\tau/a \gg 1$  (sections V–VII), the cytoplasm behaves as an unrelaxed elastic material; when the experimental timescale is much shorter than the viscoelastic relaxation time, the cytoskeleton is not able to reorganize, slide or fracture, and thus no viscoelastic dissipation can occur. Likewise, when  $Va/D \ll 1$  (sections IV and VII), the cytoplasm is highly compressible, because when the experimental timescale is much longer than the poroelastic relaxation time the infiltrated fluid in cells migrates around freely, which corresponds to significant volumetric changes. In this case, the apparent bulk modulus equals the bulk modulus of solid part of the cytoplasm, which can be characterized as highly compressible. As  $Va/D \sim 1$  (sections III and VI), poroelasticity contributes to the size-dependent mechanical properties of the cytoplasm. When  $Va/D \gg 1$  (sections II and V), the experimental condition requires large loading size and high loading speed, which cannot be achieved with optical tweezers in the cytoplasm. However, based on our experimental results in other regions of the state diagram and theoretical analysis in the framework of poroelasticity, it is clear that the loading timescale is too short compared with the poroelastic relaxation time in these two regions, and thus the intracellular fluid is trapped in the porous cytoskeleton; in this condition, there are no volumetric changes and thus it can be characterized as incompressible, with a bulk modulus significantly larger than its shear modulus. Interestingly, the cytoplasm also exhibits a pure elastic behavior when the dimensionless parameter  $V/a$  is very large, and  $Va$  is either very large (section V) or small (section VII). In these two regimes further change in the bead diameter and speed does not alter the resultant normalized force-displacement curve, as shown in Fig. S8, indicating a size- and rate-independent elastic behavior. We also note that in section VIII the probe is equal to or smaller than the typical cytoskeletal mesh size [ $\sim 50 \text{ nm}$  (19)], and thus a continuum mechanics model does not apply here.

This state diagram illustrates different characteristics and origins of cytoplasmic mechanics upon varying characteristic size and



**Fig. 5.** The state diagram of living mammalian cytoplasm as a function of two dimensionless numbers,  $V\tau/a$  and  $Va/D$ . The state diagram shows that as dimensionless number  $V\tau/a$  increases from  $10^{-2}$  to  $10^2$  the cytoplasm changes from a viscous fluid to a solid; as dimensionless number  $Va/D$  increases from  $10^{-3}$  to  $10^1$  the cytoplasm changes from a compressible material to an incompressible material. Each data point represents an experimental test with that particular speed and size combination. Different symbol shapes of the data points represent different origins of the mechanical resistance, and the color of the symbol represents the value of the measured apparent modulus. Based on our experiments at different loading speeds and probe sizes, combined with our scaling analysis, the origins of mechanical resistance in the cytoplasm can be divided into eight regions of the state diagram: I, Viscous fluid; the resistance remains a constant as displacement increases (Fig. S4). II, Incompressible viscoelasticity. III, Poroelasticity, where both viscoelasticity and poroelasticity are important (Fig. S7). IV, Compressible viscoelasticity. V, Incompressible pure elasticity; both viscoelasticity and poroelasticity do not relax in this region, and thus the cytoplasmic modulus always remains constant. VI, Poroelasticity. VII, Compressible pure elasticity (Fig. S8); poroelasticity relaxes completely while viscoelasticity does not relax at all in this region. VIII, Continuous mechanics fails when the object is equal or smaller than cytoskeletal mesh size ( $\sim 50 \text{ nm}$ ). Moreover, we mark a variety of physiological intracellular transport and cellular movement phenomena on the state diagram, to illustrate different origins of the mechanical resistance each of these processes experiences. The characteristic size and speed of these phenomena are taken from literature (details in Table S2). The dashed lines in the state diagram are transitional boundaries of different regions; the location of these dashed lines is determined by experimental results and theoretical analysis.

speed. Based on this diagram we can distinguish the origin of mechanical resistance that a variety of physiological processes experience in mammalian cytoplasm. There are many different organelles that are constantly moving in the cytoplasm; the mechanical nature of the resistance that each of them typically experiences also depends on their sizes and speeds. Using typical organelle size and speed reported previously in the literature (details in Table S2), we calculate the values of the two dimensionless numbers for movement of cell nucleus, mitochondria, and lysosome, as well as contraction of myocyte; the values of these two dimensionless numbers determine the specific region that each process typically locates on the state diagram (Fig. 5). This result reveals the underlying origins of the mechanical resistance of different cellular processes over a broad range of speed and size scales.

## Conclusion

By combining unidirectional force-displacement measurement in living mammalian cytoplasm using optical tweezers and simple scaling analysis we present a method to distinguish different origins

of cytoplasmic mechanical resistance upon intracellular transport. Using this method, we reveal that the cytoplasmic mechanical resistance can originate from the effect of either viscosity, viscoelasticity, poroelasticity, or pure elasticity depending on the speed and size of the object. As a result, the mechanical resistance and the apparent cytoplasmic modulus depend on both the speed and size of the probe and, more interestingly, in different fashions while different mechanisms dominate the apparent cytoplasmic mechanical properties. Furthermore, we summarize different cytoplasmic mechanical behaviors into a state diagram as a function of two dimensionless parameters; this state diagram shows that living mammalian cytoplasm changes from a viscous fluid to an elastic solid as one dimensionless parameter,  $V\tau/a$ , increases, and from a compressible material to an incompressible material as another dimensionless parameter,  $Va/D$ , increases. Both the cytoskeleton and bioactive cellular motors can directly regulate the viscoelastic relaxation time  $\tau$  as well as the poroelastic diffusivity  $D$  and, therefore, they can both affect the transition between different mechanical states. Our cytoplasmic state diagram provides insights into understanding the underlying mechanical nature of a variety of intracellular transport and other cellular processes, over a broad

range of speed and size scales. This state diagram can also be extended to characterize the mechanical behavior of other soft materials with both viscoelastic and poroelastic nature.

## Materials and Methods

Full materials and methods are described in *SI Materials and Methods*. Briefly, to investigate the mechanical resistance that intracellular objects experience within a living mammalian cytoplasm, we deliver micrometer-sized polystyrene beads into living NRK or HeLa cells through endocytosis. These beads, with sizes ranging from 0.5  $\mu\text{m}$  to 1.5  $\mu\text{m}$ , distribute randomly inside the cell. To obtain the force-displacement curve in the cytoplasm we use optical tweezers to trap and pull a bead unidirectionally with a constant speed toward the cell boundary. The trap stiffness is 0.05 pN/nm as determined using the traditional power spectrum method with the same type of beads in a 41% sucrose solution having a refractive index matched with that of the cell (37). To avoid any interactions with the mechanically distinct cell cortex and nucleus we only use beads that are positioned greater than 1.5  $\mu\text{m}$  away from the cell boundary, and away from both the thin lamellar region and the nucleus.

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